

FIG. 1

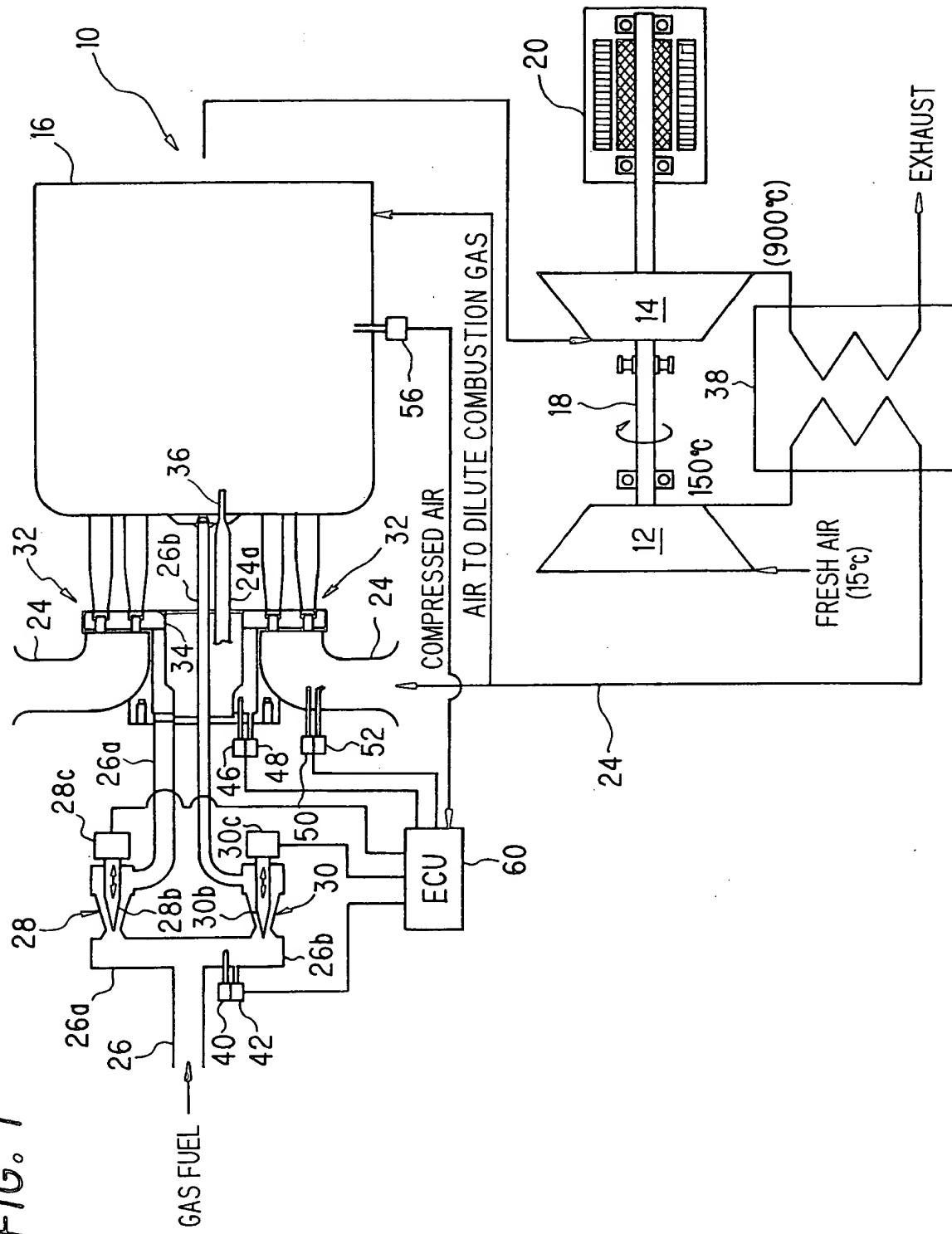


FIG. 2

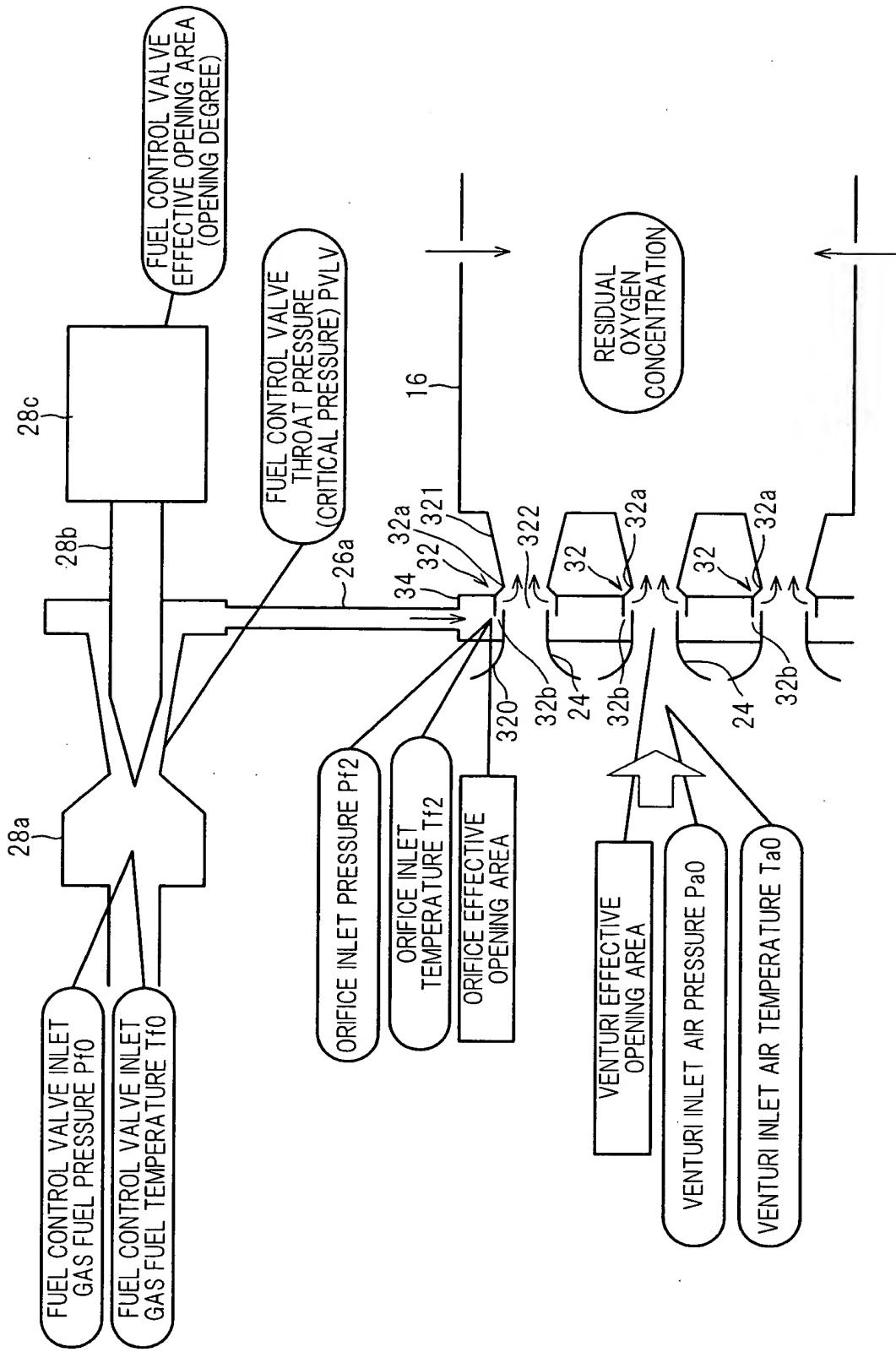


FIG. 3

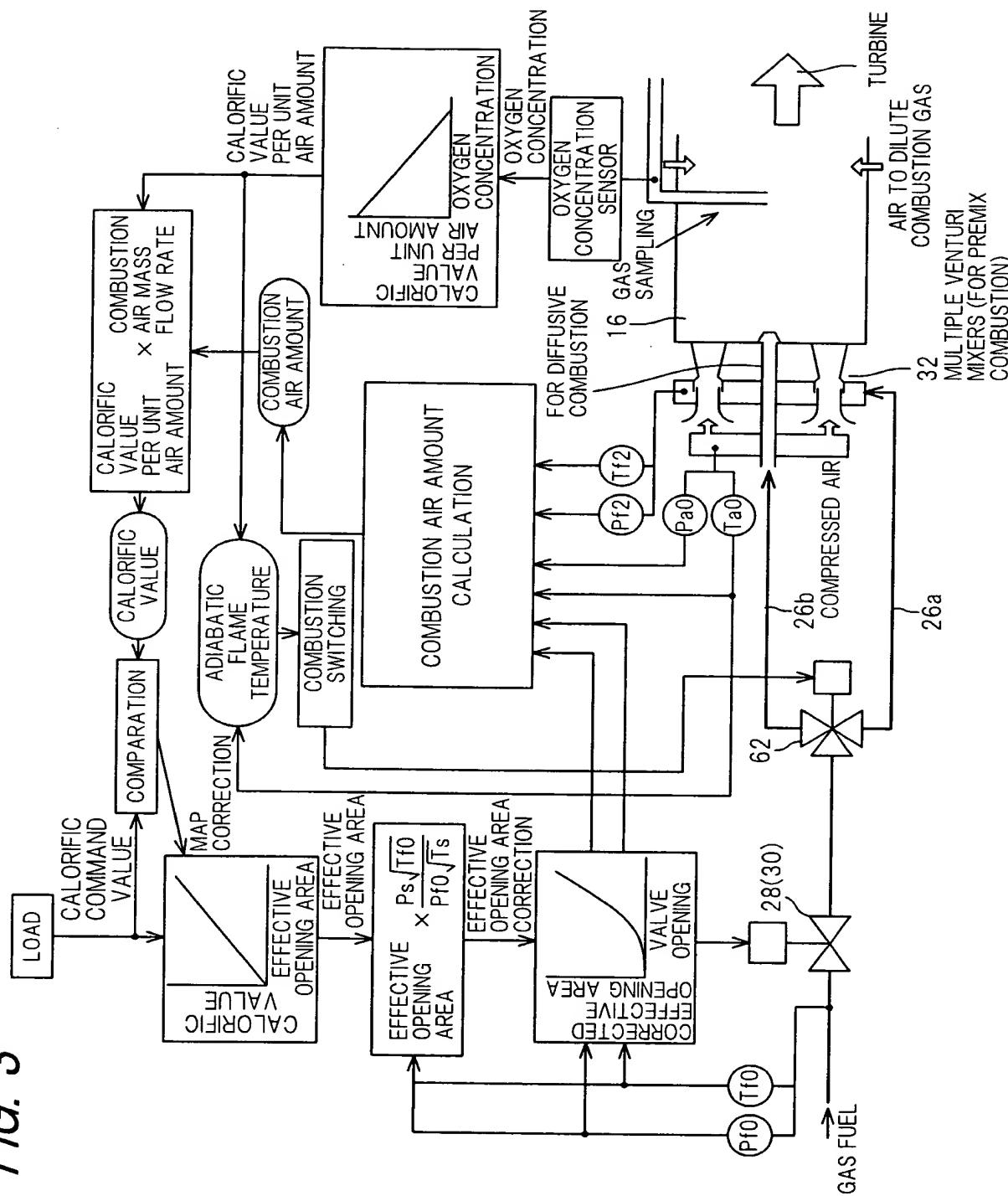
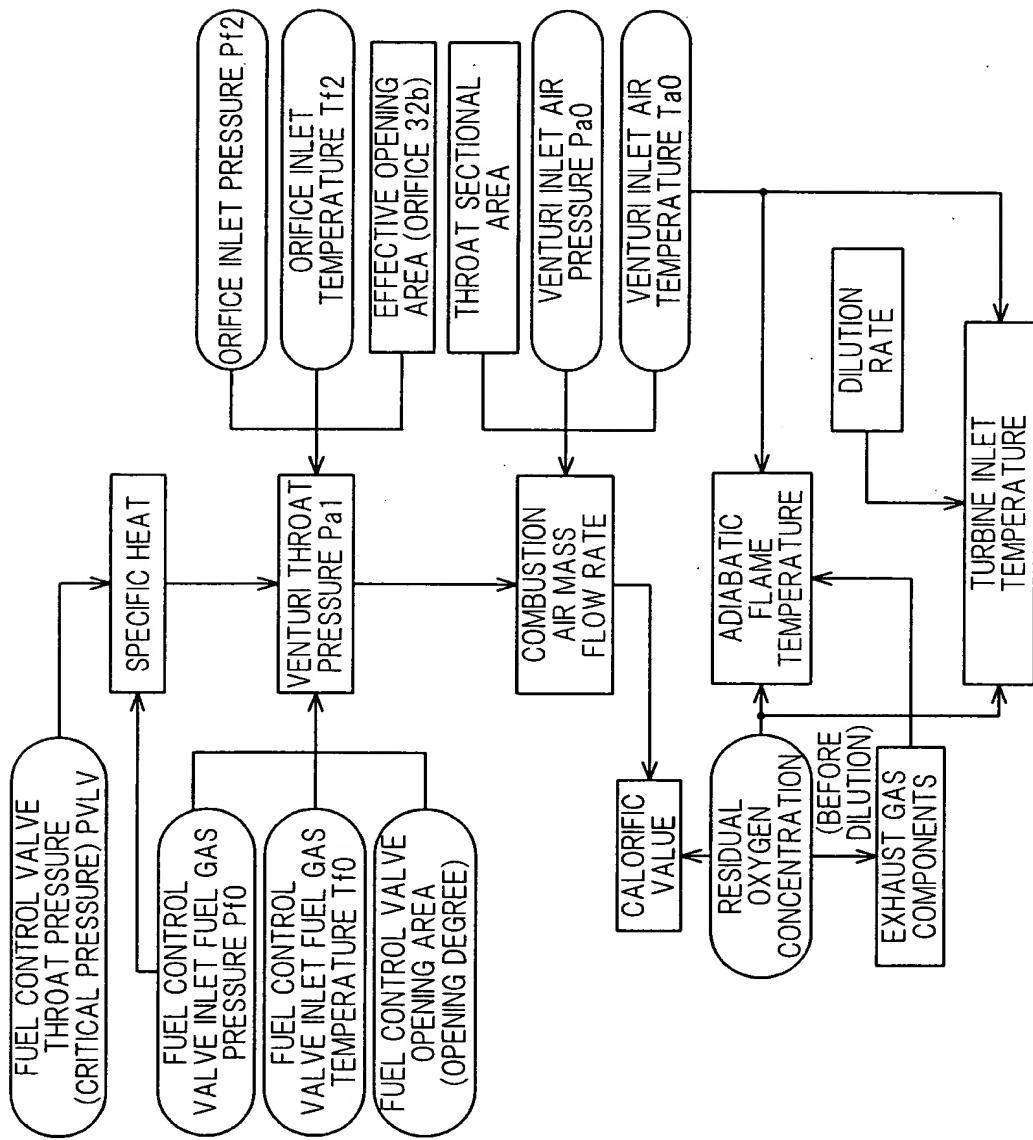


FIG. 4



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FIG. 5

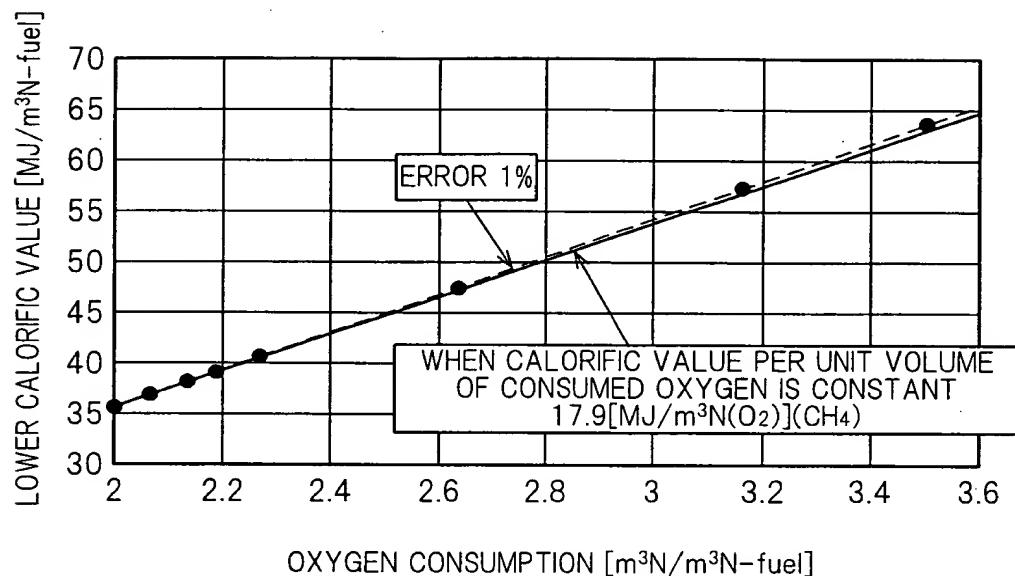


FIG. 6

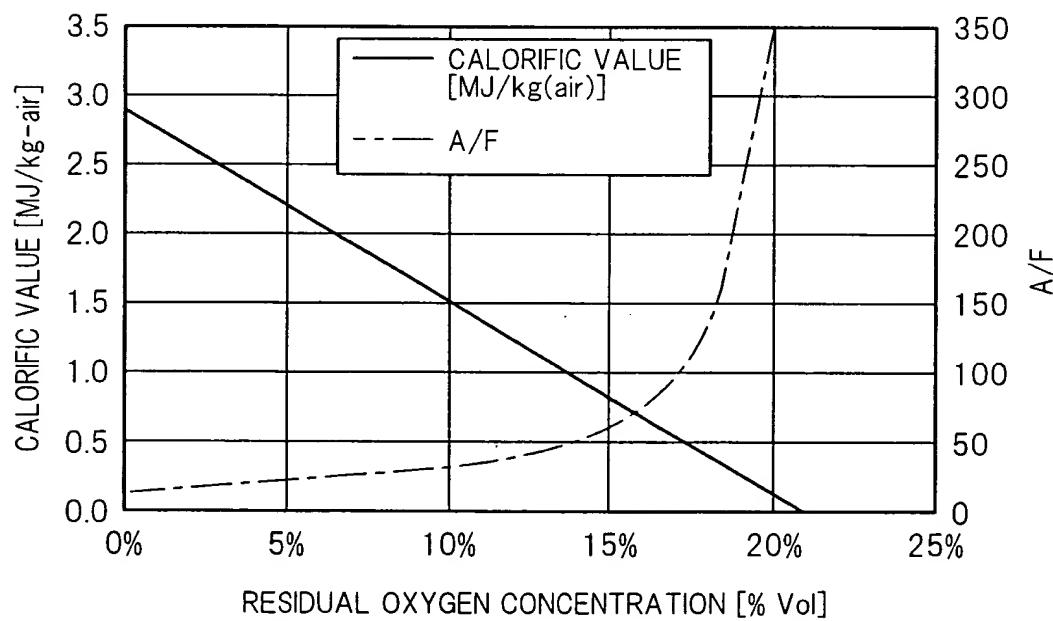
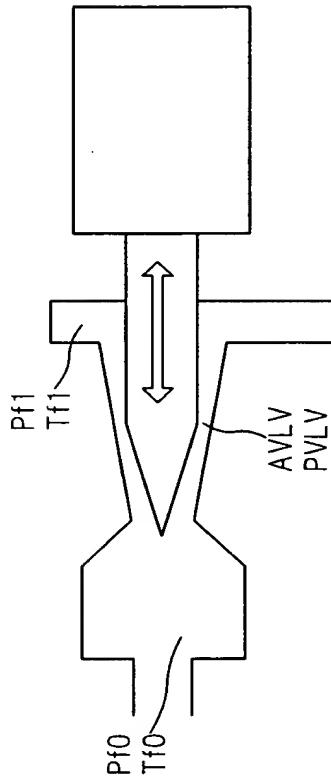


FIG. 7



$$mf = \frac{Pf2 Af}{\sqrt{R Tf2}} \left[\frac{2 \kappa_f}{\kappa_{f-1}} \left\{ \left(\frac{P_{a1}}{P_{f2}} \right)^{\frac{2}{\kappa_f}} - \left(\frac{P_{a1}}{P_{f2}} \right)^{\frac{\kappa_{f+1}}{\kappa_f}} \right\} \right]$$

$$ma = \frac{P_{a0} Aa}{\sqrt{R_a T_{a0}}} \left[\frac{2 \kappa_a}{\kappa_{a-1}} \left\{ \left(\frac{P_{a0}}{P_{a1}} \right)^{\frac{2}{\kappa_a}} - \left(\frac{P_{a0}}{P_{a1}} \right)^{\frac{\kappa_{a+1}}{\kappa_a}} \right\} \right]$$

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Pf0 : FUEL CONTROL VALVE INLET PRESSURE [Pa]

Pf2 : ORIFICE INLET PRESSURE [Pa]

PVLV : FUEL CONTROL VALVE THROAT PRESSURE [Pa]

Pa0 : VENTURI INLET AIR PRESSURE [Pa]

Pa1 : VENTURI THROAT PRESSURE [Pa]

Pf : FUEL CONTROL VALVE INLET TEMPERATURE [K]

Tf2 : ORIFICE INLET TEMPERATURE [K]

Ta0 : VENTURI INLET AIR TEMPERATURE [K].

mf : FUEL MASS FLOW RATE [kg/sec]

ma : AIR MASS FLOW RATE [kg/sec]

AVLV : FUEL CONTROL VALVE EFFECTIVE OPENING AREA [m²]

Af : ORIFICE INLET EFFECTIVE OPENING AREA [m²]

Aa : VENTURI THROAT EFFECTIVE OPENING AREA [m²]

Rf : FUEL GAS CONSTANT [kJ/kg K]

Ra : AIR GAS CONSTANT [kJ/kg K]

κf : FUEL GAS SPECIFIC HEAT

κa : AIR SPECIFIC HEAT

FIG. 8

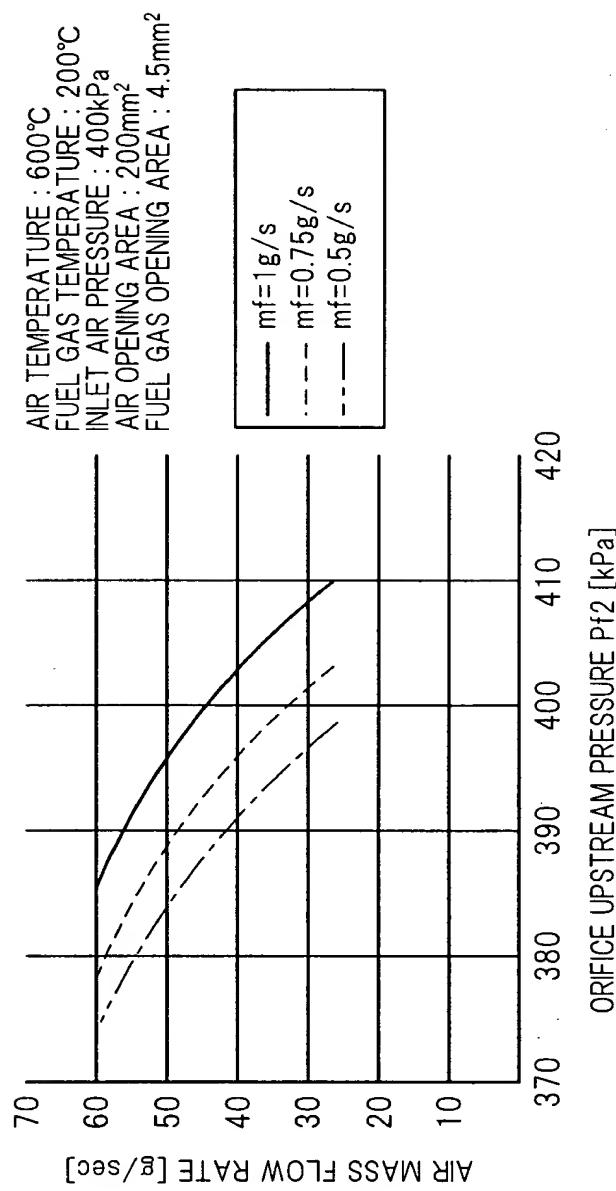


FIG. 9

$$m_{fv} = \frac{P_{f0} AVL}{\sqrt{RT_{f0}}} M \sqrt{\kappa_f} \left(1 + \frac{\kappa_{f-1}}{2} M^2 \right)^{\frac{\kappa_{f+1}}{2(\kappa_{f-1})}}$$

$$m_{f0} = \frac{P_{f2} A_f}{\sqrt{RT_{f2}}} \sqrt{\frac{2 \kappa_f}{\kappa_{f-1}} \left\{ \left(\frac{P_{a1}}{P_{f2}} \right)^{\frac{2}{\kappa_f}} - \left(\frac{P_{a1}}{P_{f2}} \right)^{\frac{\kappa_{f+1}}{\kappa_f}} \right\}}$$

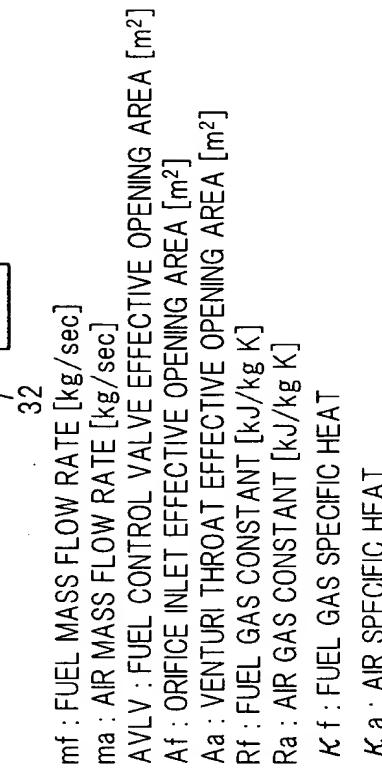
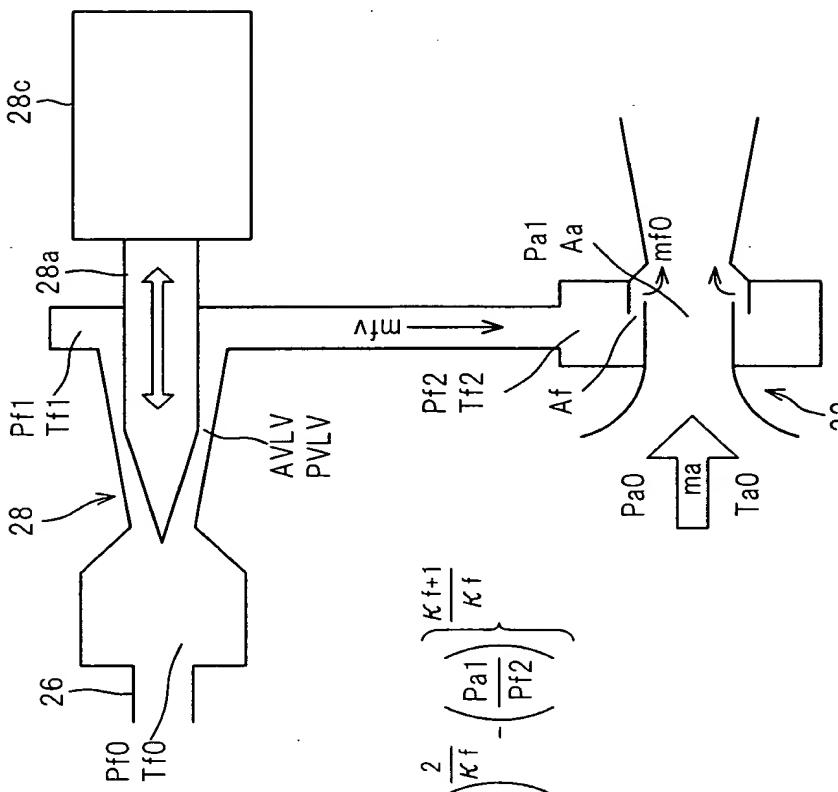
SINCE VALVE IS CHOKE-FLOW RATE VALVE, MACH IS 1, THIS YIELDS FOLLOWING

$$= \frac{P_{f0} AVL \sqrt{f_2}}{\sqrt{f_0} P_{f2} A_f} \sqrt{\kappa_f} \left(1 + \frac{\kappa_{f-1}}{2} \right)^{\frac{\kappa_{f+1}}{2(\kappa_{f-1})}}$$

$$= \frac{\kappa_{f-1}}{2 \kappa_f} = \left\{ \left(\frac{P_{a1}}{P_{f2}} \right)^{\frac{2}{\kappa_f}} - \left(\frac{P_{a1}}{P_{f2}} \right)^{\frac{\kappa_{f+1}}{\kappa_f}} \right\}$$

$$m_a = \frac{P_{a0} A_a}{\sqrt{R_a T_{a0}}} \sqrt{\frac{2 \kappa_a}{\kappa_{a-1}} \left\{ \left(\frac{P_{a0}}{P_{a1}} \right)^{\frac{2}{\kappa_a}} - \left(\frac{P_{a0}}{P_{a1}} \right)^{\frac{\kappa_{a+1}}{\kappa_a}} \right\}}$$

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P_{f0} : FUEL CONTROL VALVE INLET PRESSURE [Pa]

P_{f2} : ORIFICE INLET PRESSURE [Pa]

PVLV : FUEL CONTROL VALVE THROAT PRESSURE [Pa]

Pa0 : VENTURI INLET AIR PRESSURE [Pa]

Pa1 : VENTURI THROAT PRESSURE [Pa]

Tf0 : FUEL CONTROL VALVE INLET TEMPERATURE [K]

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Af : ORIFICE INLET EFFECTIVE OPENING AREA [m²]

Aa : VENTURI THROAT EFFECTIVE OPENING AREA [m²]

Rf : FUEL GAS CONSTANT [kJ/kg K]

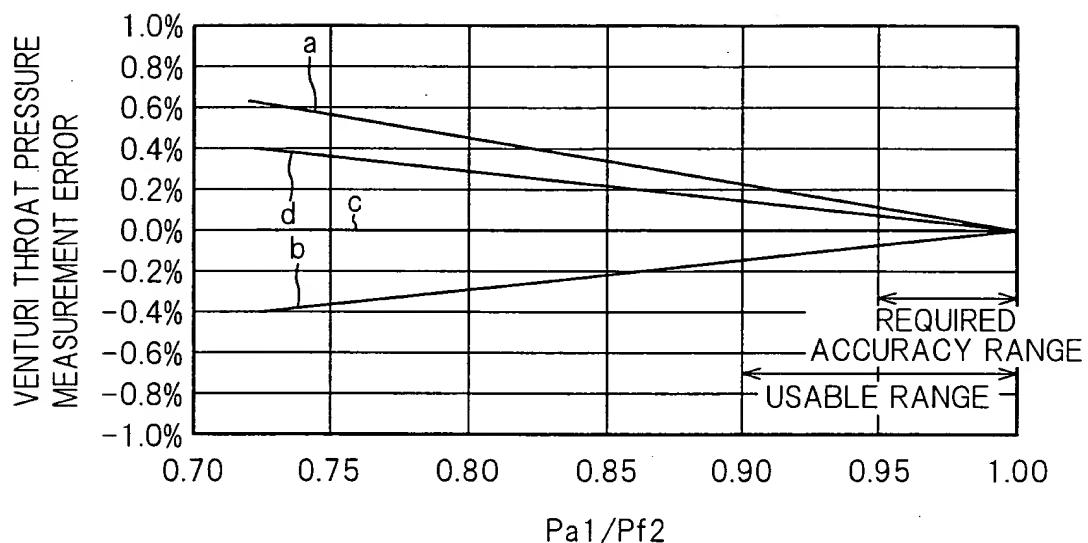
Ra : AIR GAS CONSTANT [kJ/kg K]

K_f : FUEL GAS SPECIFIC HEAT

K_a : AIR SPECIFIC HEAT

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FIG. 10



SAMPLES	SPECIFIC HEAT
a	1.309
b	1.251
c	1.274
d	1.296

FIG. 11

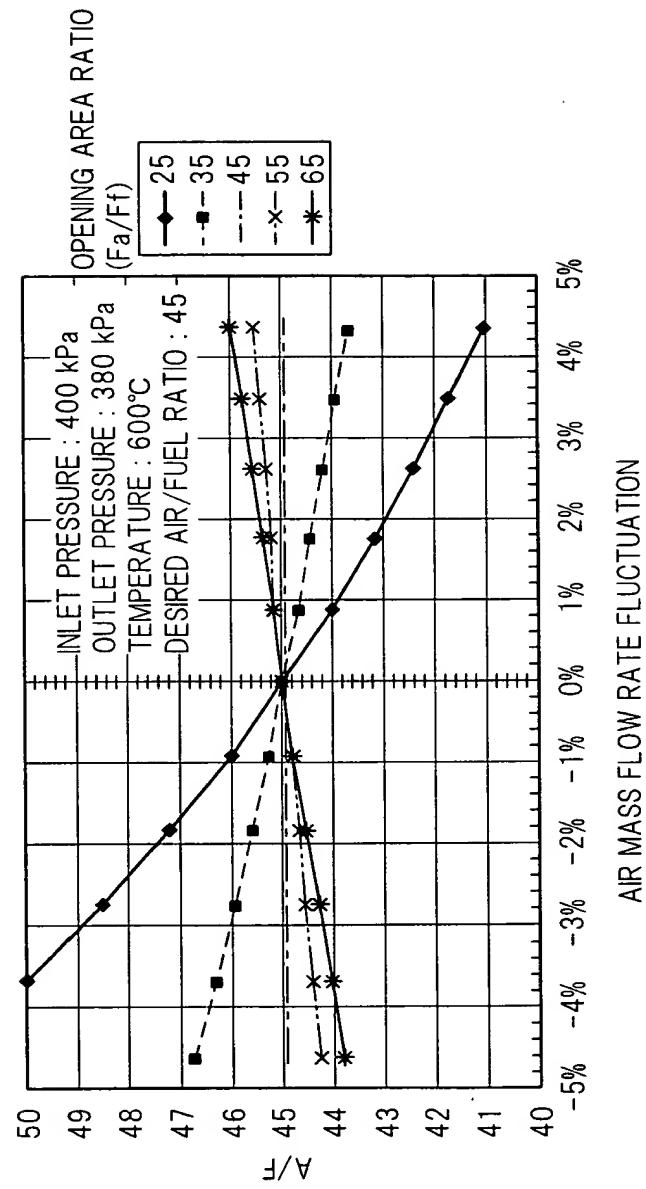
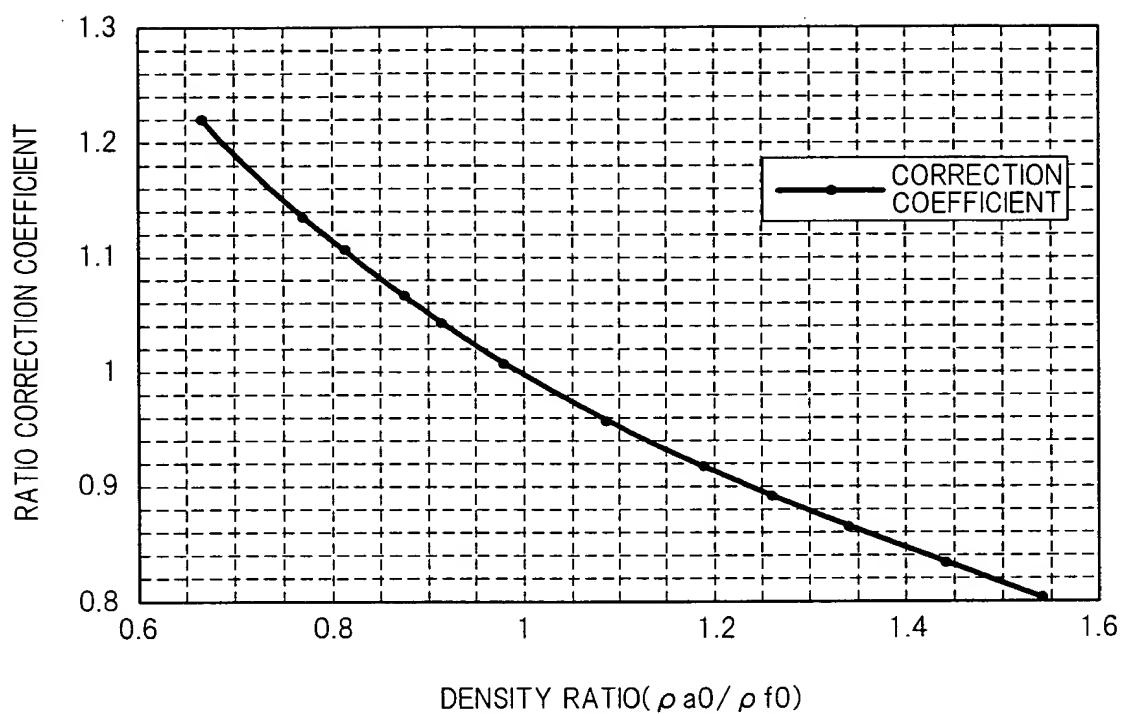


FIG. 12



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FIG. 13

